

EFFECT OF FINITE PERTURBATIONS ON STABILITY OF HARTMANN FLOW  
OF VISCOPLASTIC FLUID

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The stability of a flow of a conducting viscous plastic under small disturbances in a perpendicular magnetic field is investigated in [1]. It was shown that Hartmann flow of a viscous plastic is stable under disturbances of infinitely small amplitude of  $Ha < Ha_* = 6.5$ , while stability is lost if  $Ha > Ha_*$ .

In the present paper we consider the stability of a flow of a conducting viscoplastic fluid in a perpendicular magnetic field under disturbances of finite amplitude.

An unsteady flow of a viscoplastic fluid in a magnetic field is described by the equations of magnetohydrodynamics [2]:

$$\rho \left( \frac{\partial}{\partial t} + \mathbf{u} \nabla \right) \mathbf{u} = -\nabla p + \nabla \sigma_{ij} + \frac{1}{\mu_0} [(\nabla \times \mathbf{B}) \times \mathbf{B}];$$

$$\frac{\partial \mathbf{B}}{\partial t} = [\nabla \times (\mathbf{u} \times \mathbf{B})] + \frac{1}{\mu_0 \sigma} \Delta \mathbf{B},$$
(1)

where  $\sigma$  is the conductivity of the medium,  $\rho$  is the density, and  $\mu_0$  is the magnetic permeability. The deviator of the stress tensor  $\sigma_{ij}$  is defined in accordance with the rheological equation of a viscoplastic medium [3]:

$$\sigma_{ij} = 2 \left( \mu + \frac{\tau_0}{\sqrt{2f_{lm}f_{lm}}} \right) f_{ij} \quad \text{for} \quad \sqrt{\sigma_{lm}\sigma_{lm}} \geq \tau_0;$$

$$f_{ij} = 0 \quad \text{for} \quad \sqrt{\sigma_{lm}\sigma_{lm}} < \tau_0,$$
(2)

where  $f_{ij} = \frac{1}{2}[(\partial u_i/\partial x_j) + (\partial u_j/\partial x_i)]$  is the strain-rate tensor,  $\mu$  is the coefficient of dynamic viscosity, and  $\tau_0$  is the yield point (the limiting case  $\tau_0 \rightarrow 0$  corresponds to the case of a Newtonian fluid).

We introduce the following as characteristic quantities: the half-width of the channel  $L$ ; the velocity  $u^0 = [-\partial p/\partial x + \sigma E_0 B_0] L^2/2\mu$ ; and the external magnetic field  $B_0$ . For a steady isotropic flow in a planar channel ( $-1 \leq y \leq 1$ ) in a transverse magnetic field, we then obtain the following symmetric distribution of the dimensionless velocity [4]:

$$u_0(y) = \begin{cases} \frac{2}{Ha^2} \left[ 1 - \frac{\text{ch} Ha (\xi + y)}{\text{ch} Ha (1 - \xi)} \right] & \text{for } -1 \leq y \leq -\xi; \\ \frac{2}{Ha^2} \left[ 1 - \frac{1}{\text{ch} Ha (1 - \xi)} \right] & \text{for } -\xi \leq y \leq 0, \end{cases}$$
(3)

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where  $\xi$  is the dimensionless half-width of the quasisolid zone, determined from the transcendental equation

$$\operatorname{ch} Ha(1-\xi) = 2\xi/\kappa. \quad (4)$$

Here  $Ha = B_0 L \sqrt{\sigma/\mu}$  is the Hartmann number and  $\kappa = \tau_0 L / \mu_0 U^0$  is a dimensionless parameter characterizing the plastic properties of the viscous plastic.

We assume that the following dimensionless perturbations of the velocity and magnetic field are imposed on flow (3):

$$\begin{aligned} \varphi(x, y, t) &= \varphi_0(y) + 1/2a[\varphi(y)e^{i\alpha(x-ct)} + \tilde{\varphi}(y)e^{-i\alpha(x-ct)}]; \\ \psi(x, y, t) &= \psi_0(y) + 1/2a[\psi(y)e^{i\alpha(x-ct)} + \tilde{\psi}(y)e^{-i\alpha(x-ct)}]. \end{aligned} \quad (5)$$

Here  $\alpha$  and  $\alpha c$  are the wave number and complex frequency of the disturbances;  $\alpha$  is the amplitude of the nonstationary part of the disturbances; The functions  $\varphi_0(y)$  and  $\psi_0(y)$  define, respectively, the stationary distortion of the velocity profile of main flow (3) and of the induced magnetic field caused by the finite disturbance, while the functions  $\varphi(y)$  and  $\psi(y)$  denote, respectively, the distributions of the nonstationary parts of the perturbations of velocity and magnetic field across the channel; the sign  $\sim$  denotes the complex conjugate.

We assume that the pressure gradient averaged over a period  $\langle \partial p / \partial x \rangle$  equals the pressure gradient of the undisturbed flow. Then, inserting (5) into the basic system of equations of magnetic rheodynamics (1), we obtain, accurate to terms of order  $\alpha^2$  but allowing for terms of order  $\alpha^2 \operatorname{Re}$ , the following system of equations for  $\varphi_0(y)$ ,  $\psi_0(y)$ ,  $\varphi(y)$ , and  $\psi(y)$ :

$$\begin{aligned} \mathfrak{L}\varphi + \frac{4\alpha^2\kappa}{i\alpha \operatorname{Re}} D[D\varphi(Du)^{-1}] &= \frac{iHa^2}{\alpha \operatorname{Re}} D^2\varphi; \\ \operatorname{Re}^{-1} D^3\varphi_0(y) + \operatorname{Al} D^2\psi_0(y) &= 1/4i\alpha a^2 D[(\tilde{\varphi}D\varphi - \varphi D\tilde{\varphi}) - \operatorname{Al}(\tilde{\psi}D\psi - \psi D\tilde{\psi})]; \\ i(\alpha \operatorname{Re}_m)^{-1} [(D^2 - \alpha^2) - (u-c)]\psi &= (D + i\alpha B)\varphi; \\ \operatorname{Re}_m^{-1} D^3\psi_0(y) - D^2\varphi_0(y) &= 1/4i\alpha a^2 D^2(\tilde{\varphi}\psi - \varphi\tilde{\psi}); \\ u = u_0(y) + D\varphi_0(y); \quad B = B(y) + D\psi_0(y); \end{aligned} \quad (6)$$

here

$$\mathfrak{L} \equiv (u-c)(D^2 - \alpha^2) - D^2u + i(\alpha \operatorname{Re})^{-1}(D^2 - \alpha^2)$$

is the Orr-Sommerfeld operator;  $\operatorname{Re} = \rho u^0 L / \mu$  is the Reynolds number;  $\operatorname{Al} = B_0^2 / \mu_0 \rho u^{02}$  is the Alfvén number;  $\operatorname{Re}_m = \mu_0 \sigma u^0 L$  is the magnetic Reynolds number; and  $D \equiv d/dy$ . If  $\operatorname{Re}_m \ll 1$ , magnetic field perturbations can be neglected compared with velocity perturbations, and system (6) acquires the form

$$\mathfrak{L}\varphi + \frac{4\alpha^2\kappa}{i\alpha \operatorname{Re}} D[D\varphi(Du)^{-1}] = \frac{iHa}{\alpha \operatorname{Re}} D^2\varphi; \quad (7)$$

$$1/4i\alpha a^2 \operatorname{Re} D(\tilde{\varphi}D\varphi - \varphi D\tilde{\varphi}) = D^3\varphi_0(y). \quad (8)$$

The functions  $\varphi_0(y)$  and  $\varphi(y)$  must satisfy the "no-slip" conditions on the solid surface of the channel ( $y = -1$ ):

$$D\varphi_0(-1) = 0; \quad \varphi(-1) = D\varphi(-1) = 0. \quad (9), (10)$$

Disturbance of main flow (3) leads to a deformation of the surface separating the zones of quasisolid and viscous flows. For a mean pressure gradient over the length of the channel ( $\langle dp/dx \rangle = \text{const}$ ) equal to the pressure gradient of the undisturbed flow, the expression for deformation of the surface separating the zones has the form

$$y = -\xi + \frac{a}{2} [h e^{i\alpha(x-ct)} + \tilde{h} e^{-i\alpha(x-ct)}], \quad (11)$$

where  $h = -\varphi''(-\xi) [u''(-\xi)]^{-1}$  is the deformation of the separating surface [5].

Perturbations of velocity and the strain-rate tensor  $f_{ij}$  reduce to zero on the boundary of the quasisolid zone  $f_{ij} = 0$ . These conditions, written on the mean surface separating the zones  $y = -\xi$ , have the following form [5], accurate to terms of order  $\alpha^2$ :

$$\varphi_0(-\xi) = 0; \quad \varphi(-\xi) = \varphi'(-\xi) = 0. \quad (12), (13)$$

We introduce a new independent variable  $z = (y + \xi)/(1 - \xi)$ , and at the same time we change the characteristic length  $L$  and velocity  $u^0$  to  $L_1 = L(1 - \xi)$  and  $u_1 = U^0 \{(2/Ha^2)[1 - (1/\cosh Ha(1 - \xi))]\}$ . The problem is then reduced to investigating the stability of a Hartmann flow under finite disturbances [6]:

$$u_0(y) = \frac{\text{ch } Ha_1 - \text{ch } Ha_1 z}{1 - \text{ch } Ha_1}; \quad Ha_1 = B_0 L_1 \sqrt{\frac{\sigma}{\mu}}. \quad (14)$$

Let us consider the solution of system (7), (8) subject to boundary conditions (9)-(13). The function  $\varphi(z)$  is determined from the problem (7), (10), (13). The first pair of independent particular solutions  $\varphi_1$  and  $\varphi_2$  can be represented in the form of power series [5]:

$$\varphi_1 = (z - z_c) \sum_{k=1}^{\infty} a_k (z - z_c)^{k-1}; \quad \varphi_2 = P_c \ln(z - z_c) + \sum_{k=0}^{\infty} b_k (z - z_c)^k. \quad (15)$$

Here  $z_c$  is the point at which  $u(z_c) = \Re c c$ ,  $P_c = D^2 u(z_c) / Du(z_c) - 2a_2 = 2b$ ;  $z_c$  will be regarded as an independent parameter defining the coefficients in expansions (15). The second pair of independent particular solutions  $\varphi_{3,4}$  (viscous integrals [7]) we take in the form

$$\varphi_{3,4} = \int_{\pm\infty}^{\eta} d\eta \int_{\pm\infty}^{\eta} \sqrt{\eta} H_{\frac{1}{2}}^{(1,2)} \left[ \frac{2}{3} (i\eta)^{3/2} \right] d\eta; \quad (16)$$

$$\eta = (z - z_c) \varepsilon, \quad \varepsilon = (\alpha \text{Re } u_c')^{1/2}.$$

When constructing the solutions of Eq. (7), it must be remembered that the point  $z = 0$  is a singular point of Eq. (7), since  $u'(0) = 0$ . Accordingly, in the neighborhood of the point  $z = -\sigma + O(\gamma)$ ,  $\gamma = \kappa(\alpha \text{Re})^{-1/2}$ , where the plastic properties manifest themselves, we transform Eq. (7) by means of a new independent variable  $t = z\gamma^{-1}$  to the form [1]

$$\varphi^{IV} + \frac{A_1}{t} \varphi'' + \frac{A_2}{t^2} \varphi' + A_3 \varphi = 0. \quad (17)$$

Here the  $A_i$  are regular functions of  $t$ .

For  $t \in [0, t_s]$ ,  $t_s = z_s \gamma^{-1} \sim O(1)$ , the quantity  $A_3 \approx 0$  and the solutions of (17) have the form

$$\varphi_1^* = \text{const}; \quad \varphi_2^* = \sum_{k=0}^{\infty} \frac{\alpha_k t^{k+3}}{k+3}; \quad \varphi_3^* = \sum_{k=0}^{\infty} \frac{\beta_k t^{k+2}}{k+2}; \quad (18)$$

$$\varphi_4^* = \int \varphi_3^* \ln t \, dt + \sum_{k=0}^{\infty} \frac{\gamma_k t^{k+1}}{k+1},$$

where  $\alpha_k$ ,  $\beta_k$  and  $\gamma_k$  are given by recurrence relations [1]. It follows from boundary conditions (13) that for  $t \in (0, t_s)$  the general solution of Eq. (17) has the form

$$\varphi^*(t) = C_2^* \varphi_2^* + C_3^* \varphi_3^*. \quad (19)$$

The condition that the general solution of Eq. (7) in the region  $[0, -1]$  be nontrivial, written allowing for boundary conditions (10) and (13) and for the requirement that the solutions  $\varphi$  and  $\varphi^*$  match at the point  $z = z_s$ ,

$$\frac{d^k \varphi}{dy^k}(z_s) = \frac{d^k \varphi^*}{dy^k}(z_s) \quad (k=0, 1, 2, 3), \quad (20)$$

leads, accurate to terms of order  $\propto (\alpha \text{Re})^{-1/2}$ , to the following secular equation:

$$\frac{\varphi_1(-1)\varphi_2(0) - \varphi_1(0)\varphi_2(-1)}{\varphi_2(0)\varphi_1'(-1) - \varphi_1(0)\varphi_2'(-1)} = \frac{\varphi_3(-1)}{\varphi_3'(-1)}, \quad (21)$$

which coincides in form with the secular equation in the study of the stability of a Hartmann flow with respect to antisymmetric perturbations [1].

Utilizing Eq. (8), boundary conditions (9) and (12), and the definitions of  $P_c$  and  $\varepsilon$ , we obtain the following relationships for the disturbance amplitude and the corresponding Reynolds number:

$$a^2 = \frac{(1+z_c)^3}{\eta^3} \frac{(u_c' P_c - u_c'')}{\tau_c'} u_c'; \quad (22)$$

$$\text{Re} = \frac{\eta^3}{\alpha(1+z_c)^3} \frac{(\tau_c' - P_c \tau_c)}{(u_c' \tau_c' - u_c'' \tau_c)}, \quad (23)$$

where  $\tau_c = \frac{1}{4} i [\varphi'(z_c) \bar{\varphi}(z_c) - \bar{\varphi}'(z_c) \varphi(z_c)]$ .

Here  $\text{Re} = \rho u_1 L_1 / \mu$ . If we take as the characteristic velocity of motion of the quasisolid zone  $u_1$  and as the characteristic dimension the half-width of the channel  $L$ , then the corresponding Reynolds number  $\text{Re}_* = \rho u_1 L / \mu$  and the disturbance amplitude  $\alpha_*^2$  are given by the expressions

$$\text{Re}_* = \text{Re}(1-\xi)^{-1}; \quad \alpha_*^2 = a^2(1-\xi)^{-2}. \quad (24)$$

Utilizing secular equation (21) for fixed values of the Hartmann number  $\text{Ha}_1$  and the parameter  $P_c$  to determine the values of  $\alpha$ ,  $z_c$ , and  $\varepsilon$  corresponding to neutral disturbances  $\text{Im } c = 0$ , and inserting these values into (22) and (23), we find the function  $\text{Re} = \text{Re}(\alpha, \text{Ha}_1 = \text{const})$  defining the curve of neutral stability. The results of the calculations are shown in Fig. 1, where curves 1-4 correspond to  $\text{Ha}_1 = 0$ ,  $P_c = -2.12, -2.1, -2.08, \text{ and } -2.6$ ; curves 5-8 to  $\text{Ha}_1 = 2$ ,  $P_c = -2.66, -2.64, -2.62, \text{ and } -2.6$ ; curves 9-11 to  $\text{Ha}_1 = 3$ ,  $P_c = -3.4, -3.38, \text{ and } -3.36$ ; curves 12-15 to  $\text{Ha}_1 = 4$ ,  $P_c = -5.62, -5.6, -5.48, \text{ and } -5.46$ .

Plots of the critical values of the Reynolds number  $\text{Re}_0$ , the square of the disturbance amplitude  $\alpha_0^2$ , and the wave number  $\alpha_0$  versus the Hartmann number  $\text{Ha}_1$  are shown in Fig. 2. The convergence of series (15) deteriorates greatly at large values of the Hartmann number ( $\text{Ha}_1 > 5$ ). In this case the velocity distribution in the flow becomes similar to the velocity distribution in a boundary layer of thickness  $\text{Ha}_1^{-1/2}$  with an almost uniform velocity in the center of the channel; it is given by

$$\bar{u}(z) = 1 - e^{-\delta}, \quad (25)$$

where  $\delta = \text{Ha}_1(1+z)$  for  $-1 \leq z \leq 0$ . In this case Eq. (7) can be rewritten in the form

$$\mathcal{L}\varphi + \frac{4\alpha_*^2 \kappa}{i \text{Re}^*} D[D\varphi(D\bar{u})^{-1}] = \frac{i}{\alpha_*^* \text{Re}^*} D^2\varphi, \quad (26)$$

where

$$\alpha_*^* = \alpha \text{Ha}_1^{-1}, \quad \text{Re} = \text{Re}^* \text{Ha}_1^{-1}, \quad D \equiv d/d\delta.$$

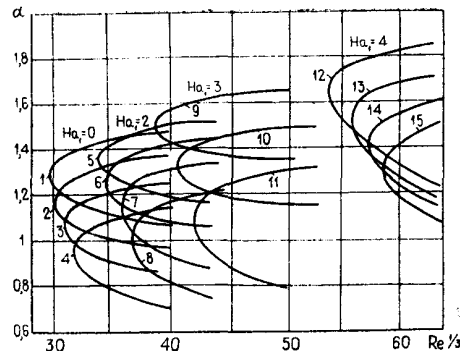


Fig. 1. Curves of neutral stability for  $\text{Ha}_1 = 0, 2, 3, \text{ and } 4$ .

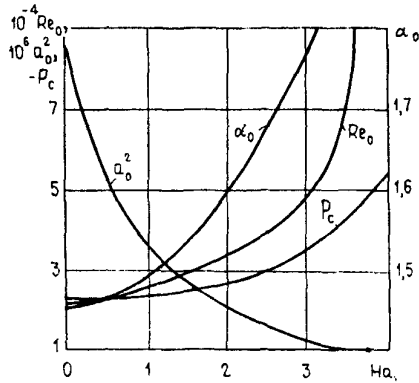


Fig. 2

Fig. 2. Dependence of critical Reynolds number  $Re_0$  and corresponding values of square of disturbance amplitude  $\alpha_0^2$ , wave number  $\alpha_0$ , and parameter  $P_c$  on Hartmann number  $Ha_1$ .

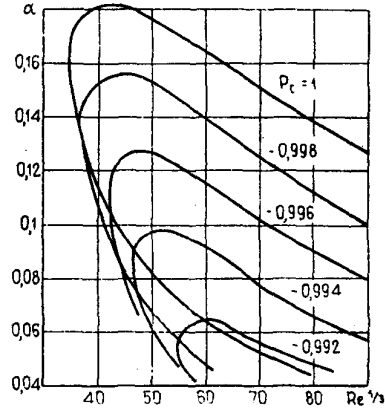


Fig. 3

Fig. 3. Curves of neutral stability for  $Ha_1 \gg 1$ .

The solutions of Eq. (26) are identical to those of Eq. (7), except that  $z$ ,  $\alpha$ , and  $Re$  are replaced by  $\delta$ ,  $\alpha^*$ , and  $Re^*$ . Under this substitution,  $z = 0$  goes over into  $\delta = Ha_1$  and for  $\delta = Ha_1 = 5$  can be regarded as the edge of the boundary layer, since for  $\delta \geq 5$  the velocity profile can be regarded with sufficient accuracy as equal to unity. On the edge of the boundary layer, we can specify the following boundary conditions:

$$\varphi' + \alpha^* \varphi = 0 \quad \text{for} \quad \delta = 5. \quad (27)$$

On the wall  $\delta = 0$  ( $z = -1$ ) we impose the standard "no-slip" conditions:

$$\varphi = D\varphi = 0. \quad (28)$$

In this case the secular equation has the following form, accurate to  $(\alpha Re)^{-1}$ :

$$\frac{\varphi_2(0)[\varphi_1'(5) + \alpha^* \varphi_1(5)] - \varphi_1(0)[\varphi_2'(5) + \alpha^* \varphi_2(5)]}{\varphi_2'(0)[\varphi_1'(5) + \alpha^* \varphi_1(5)] - \varphi_1'(0)[\varphi_2'(5) + \alpha^* \varphi_2(5)]} = \frac{\varphi_3(0)}{\varphi_3'(0)}. \quad (29)$$

Utilizing Eq. (8), boundary conditions (27) and (28), and also the definitions of  $P_c$  and  $\epsilon$ , we obtain the dependences for  $Re$  and  $\alpha^2$ .

Calculations showed that for  $Ha_1 \gg 1$  the magnetic field freezes finite disturbances, and the disturbance most dangerous as far as loss of stability is concerned are small disturbances corresponding to the linear theory. In Fig. 3 we show the curves of neutral stability for  $Ha \gg 1$  and  $P_c = -1, -0.998, -0.996, -0.994$ , and  $-0.992$ . It can be seen that the minimum Reynolds number corresponds to an undistorted velocity profile ( $P_c = -1$ ) and is given, along with the corresponding value of the wave number, by

$$Re = 5 \cdot 10^4 Ha_1 (1 - \xi)^{-1}; \quad \alpha = 0.19 Ha_1 (1 - \xi)^{-1}. \quad (30), (31)$$

The effect of finite disturbances in a strong magnetic field leads to the appearance of subcritical instability. Evidently, this is connected with the ability of a magnetic field to suppress turbulent exchange of energy between disturbances of different scales.

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